

Review

Heterogeneous and Monolithic 3D Integration Technology for Mixed-Signal ICs

Jaeyong Jeong ^{1,†}, Dae-Myeong Geum ^{2,†} and SangHyeon Kim ^{1,2,*}

¹ School of Electrical Engineering, Korea Advanced Institute of Science and Technology (KAIST), Daejeon 34141, Korea

² Information and Electronics Research Institute, Korea Advanced Institute of Science and Technology (KAIST), Daejeon 34141, Korea

* Correspondence: shkim.ee@kaist.ac.kr

† These authors contributed equally to this work.

Abstract: For next-generation system-on-chips (SoCs) in diverse applications (RF, sensor, display, etc.) which require high-performance, small form factors, and low power consumption, heterogeneous and monolithic 3D (M3D) integration employing advanced Si CMOS technology has been intriguing. To realize the M3D-based systems, it is important to take into account the relationship between the top and bottom devices in terms of thermal budget, electrical coupling, and operability when using different materials and various processes during integration and sequential fabrication. In this paper, from this perspective, we present our recent progress of III-V devices on Si bottom devices/circuits for providing informative guidelines in RF and imaging devices. Successful fabrication of the high-performance InGaAs high electron mobility transistors (HEMTs) on the bottom ICs, with a high unity current gain cutoff frequency (f_T) and unity power gain cutoff frequency (f_{MAX}) was accomplished without substrate noise. Furthermore, the insertion of an intermediate metal plate between the top and bottom devices reduced the thermal interaction. Furthermore, the InGaAs photodetectors (PDs) were monolithically integrated on Si bottom devices without thermal damage due to low process temperature. Based on the integrated devices, we successfully evaluated the device scalability using sequential fabrication and basic readout functions of integrated circuits.

Keywords: heterogeneous integration; monolithic 3D; sequential 3D; wafer bonding; RF application; image sensor; mixed-signal IC; system-on-chip



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1. Introduction

Recently, 3-dimensional (3D) integration technology has been actively investigated to overcome the disadvantages of conventional 2D integration in highly-dense device systems, such as interconnection delay and high-power consumption [1–3]. Indeed, various mixed-signal IC chips using through Si vias (TSVs) based 3D chip stacking technology have been reported in communication, image sensors, etc. [4]. For image sensors, in order to solve the image distortion for moving targets, a three-layer stacked structure consisting of photodiodes on dynamic random-access memory (DRAM) on a logic circuit demonstrated the improved frame speed rate [5]. Similarly, in communication, by using Si-interposer, and TSV, RF system-on-chips (SoCs) have been demonstrated [6–9]. However, while 3D integration technology has improved the mixed-signal IC performance, form factor, large via size, alignment accuracy, and via densities still need to be improved.

As a result, heterogeneous and monolithic 3D (M3D) integration has been extensively studied in order to maximize the benefits of 3D integration in terms of low power consumption, interconnection delay, and via densities. M3D-based RF transistors on Si CMOS ICs, high-resolution microdisplays on Si CMOS driving circuits, and imaging systems on MOSFETs and neuromorphic devices have been demonstrated [10–19]. Furthermore, the aforementioned studies demonstrated the heterogeneous integration of different materials

of III-V compound semiconductors with Si- and Ge-based bottom devices, indicating better flexibility in process design and performance improvements, as shown in Figure 1. Although the heterogeneous integration method has many advantages, thermal management on bottom devices, physical coupling, and other factors should be considered first for establishing the M3D-based device architectures.

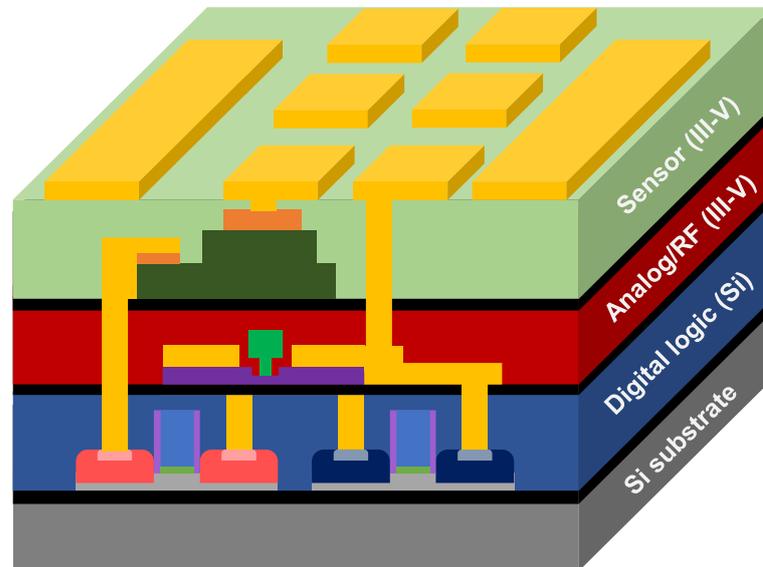


Figure 1. Conceptual illustration of heterogeneous and monolithic 3D integrated system including digital logic (blue layer, Si technology), analog/RF (red layer, III-V technology), and sensor (green layer, III-V technology).

Thus, in this paper, we present our recent research on the M3D integration of RF devices on Si CMOS circuits and InGaAs photodetectors on Si bottom FETs for realizing future M3D-based mixed signal systems. First, we discuss the improved RF device performances, noise de-coupling, and thermal coupling on Si CMOS ICs, which should be considered in future M3D-based 6G systems. Secondly, to implement high-resolution III-V image sensors, the thermal damage on bottom devices during the top device process, device scalability, and basic functionality of readout operation will be discussed in imaging devices.

2. RF System-on-Chip (SoC)

Thanks to the excellent performance improvement through scaling of Si CMOS, not only digital but also analog/RF domains were able to be successfully implemented using Si CMOS technology [20–22]. However, it is expected that next-generation wireless communication will use a frequency band of 100–300 GHz, which is challenging to implement a high-performance RF chip with only Si CMOS technology. As a result, the heterogeneous and monolithic 3D integration emerged as a promising solution to overcome the limited RF performance of Si CMOS technology and utilize the advantages of Si CMOS technology on the digital side [23–26]. Here, we discuss the heterogeneous and M3D integrated RF SoC, which contributes to optimizing performance both on digital and analog/RF and enhances the functionality.

2.1. Why Heterogeneous and Monolithic 3D Integration for RF SoC?

A lot of research has been done on RF devices using III-V HEMT, III-V HBT, SiGe HBT, and Si CMOS technology over a long period. Although the RF performance of various technologies has been improved with the scaling down of technology nodes, the III-V-based devices exhibit outstanding RF performance when compared with the other technologies due to their high electron mobility. The figure of merit (FOM) is used to estimate the performance and capabilities of various technologies. The main FOMs of RF devices are

the unity current gain cutoff frequency (f_T) and unity power gain cutoff frequency (f_{MAX}). Figure 2 shows f_T and f_{MAX} of the state-of-the-art III-V HEMT, III-V HBT, SiGe HBT, and Si CMOS. The f_T and f_{MAX} represent the frequency at which the transistor provides a unity gain. The transistor cannot provide gain at frequencies higher than f_T and f_{MAX} .

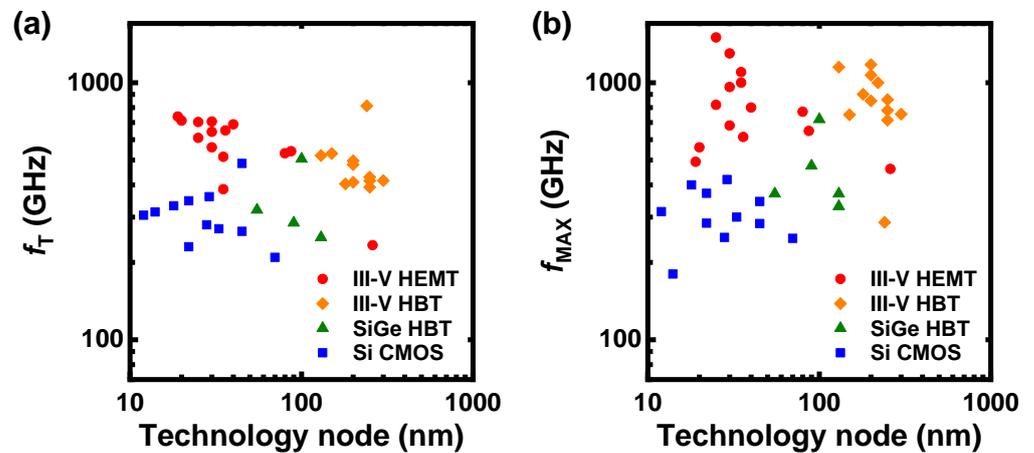


Figure 2. The (a) f_T and (b) f_{MAX} versus technology node of the state-of-the-art RF transistors.

The III-V HEMT, III-V HBT, SiGe HBT, and Si CMOS have made significant progress in the goal of increasing f_T and f_{MAX} to process more high-frequency signals. In the case of Si-based technology, the RF performance has continued to increase into the range of 300–500 GHz by technology node scaling [20–22]. For CMOS technology, as the gate length of Si MOSFET is extremely reduced, advanced structures, such as FinFETs or gate-all-around (GAA) FETs, become essential. However, these structures cause increasing parasitic capacitance [20]. Therefore, Si CMOS technology has reached the limit in which f_T and f_{MAX} do not increase even if the gate length is scaled. The SiGe HBT technology that can be integrated with Si CMOS has reached f_T of 500 and f_{MAX} of 700 [27]. Even though SiGe HBT exhibits higher f_T and f_{MAX} than that of Si CMOS, it is not enough f_T and f_{MAX} to successfully implement 6G.

On the other hand, the transistors exhibiting f_T above 700 GHz and f_{MAX} above 1.5 THz have been demonstrated with III-V-based devices, especially InGaAs-based transistors, which has never been achieved in other solid-state transistors [28–30]. Furthermore, the III-V-based RF device is the only technology option at this moment that shows a cut-off frequency (f_T and f_{MAX}) over 700 GHz, appropriate to amplify the signal between 100 and 300 GHz for future wireless communication [31]. However, despite their excellent RF performances, the III-V technology has been restricted for a long time because the III-V material cannot be simply integrated with Si CMOS technology. Integrating with Si CMOS technology is important because the RF chip needs not only RF circuits, such as low noise amplifier (LNA) and power amplifier (PA) but also the digital processor.

Therefore, to overcome the limitation of Si CMOS in high frequency and take advantage of highly advanced Si CMOS technology in digital, the heterogeneous integration of III-V and Si is required, as shown in Figure 3. In conventional heterogeneous integration, the III-V technology-based analog/RF circuits and Si CMOS technology-based digital circuits are fabricated respectively and integrated through packaging. However, the packaging technology has disadvantages, such as a long connection distance, high loss, high power consumption, and a large form factor. Furthermore, considering the development direction of the current wireless communication technology, massive multiple-input multiple-output (MIMO) and dense device integration are very important features one must take into account for hardware development [32,33]. For the application of Massive MIMO using a small antenna array, the requirement for the fine pitch size is increasing, and it is urgent to develop a technology that can achieve the micrometer level or less pitch size of I/O pins required for communication between the modules. According to the above

trend, the packaging-based integration would be facing this technical difficulty, whereas the monolithic 3D integration process would be applicable for the finer pitch size as the integration density has been proven in other various applications (ex. Logic). Therefore, heterogeneous and monolithic 3D integration is essential for future wireless communication.

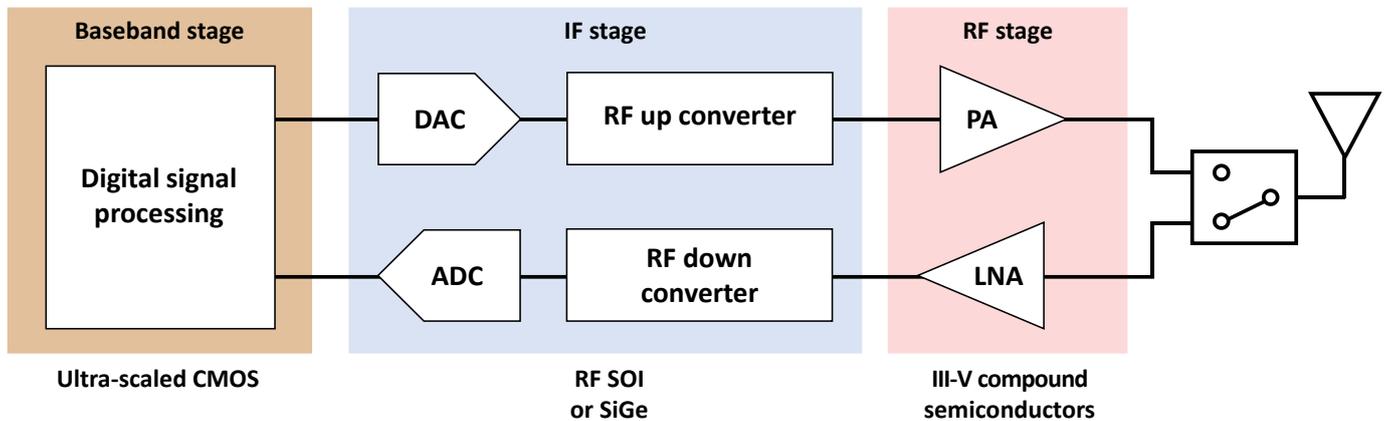


Figure 3. The strategy of heterogeneous integration in RF chips to optimize the performance in both digital and analog/RF circuits.

2.2. Heterogenous and Monolithic 3D Integration of III-V-Based RF Devices on Si CMOS

For future next-generation wireless communication, the co-integration of III-V-based RF devices and Si CMOS digital circuits is positively necessary, as shown in Figure 4a. We have successfully implemented the heterogeneous and monolithic 3D integration of III-V-based RF devices on Si CMOS by direct wafer bonding [10]. The cross-sectional SEM image is shown in Figure 4b. The III-V layers were uniformly bonded on Si CMOS. The top RF devices are based on InGaAs HEMT, and the bottom Si CMOS is a standard MOSFET structure with SiO₂ gate dielectric and poly-Si gate. The heterogeneous and monolithic 3D integration process flow consists of (1) bottom Si CMOS fabrication with 180 nm standard CMOS technology, (2) back end of line (BEOL) process, (3) III-V heterostructure transfer by wafer bonding, (4) top device fabrication, (5) interconnect between top and bottom. Such monolithic 3D integration by direct wafer bonding enables tight integration of different technologies. The process temperature after the front end of the line (FEOL) of Si CMOS is very low at 300 °C or less [10,34]. Figure 5 shows the impact of monolithic 3D integration on the performance of bottom Si CMOS. The transistor characteristics, such as subthreshold swing, on current, off current, and threshold voltage, did not change after monolithic 3D integration, as shown in Figure 5a. Not only the characteristics of the individual transistor but also the function composed of several transistors showed almost no change in characteristics, as shown in Figure 5b. The thermal budget of 3D integration and top device fabrication is 300 °C, which is suitable for monolithic 3D integration.

We showed the basic concept of heterogeneous and monolithic 3D integrated III-V-based RF devices on Si CMOS circuits, as shown in Figure 6a. The top III-V-based RF devices consist of f_T -oriented InGaAs HEMTs, which are designed to optimize the f_T characteristic and f_{MAX} -oriented InGaAs HEMTs, which are engineered to maximize the f_{MAX} characteristic and bottom Si CMOS circuits are composed of the analog-to-digital converters (ADCs) and digital-to-analog converters (DACs). The f_T -oriented InGaAs HEMT has a narrow head, and short gate stem, and the f_{MAX} -oriented InGaAs HEMT features a wide head and short gate stem. The top RF device can amplify the high-frequency signals of hundreds of GHz because the III-V-based RF devices exhibit outstanding f_T and f_{MAX} , as shown in Figure 6b. At the same time, the bottom Si CMOS circuits of ADC and DAC can convert analog and digital signals to digital and analog signals, as shown in Figure 6c–h. A key feature of our heterogeneous and monolithic 3D integrated III-V-based RF devices on Si CMOS circuits is the ability to process analog/RF signals and digital

signals with excellent performance at the same chip, utilizing different technologies (III-V and Si CMOS technology).

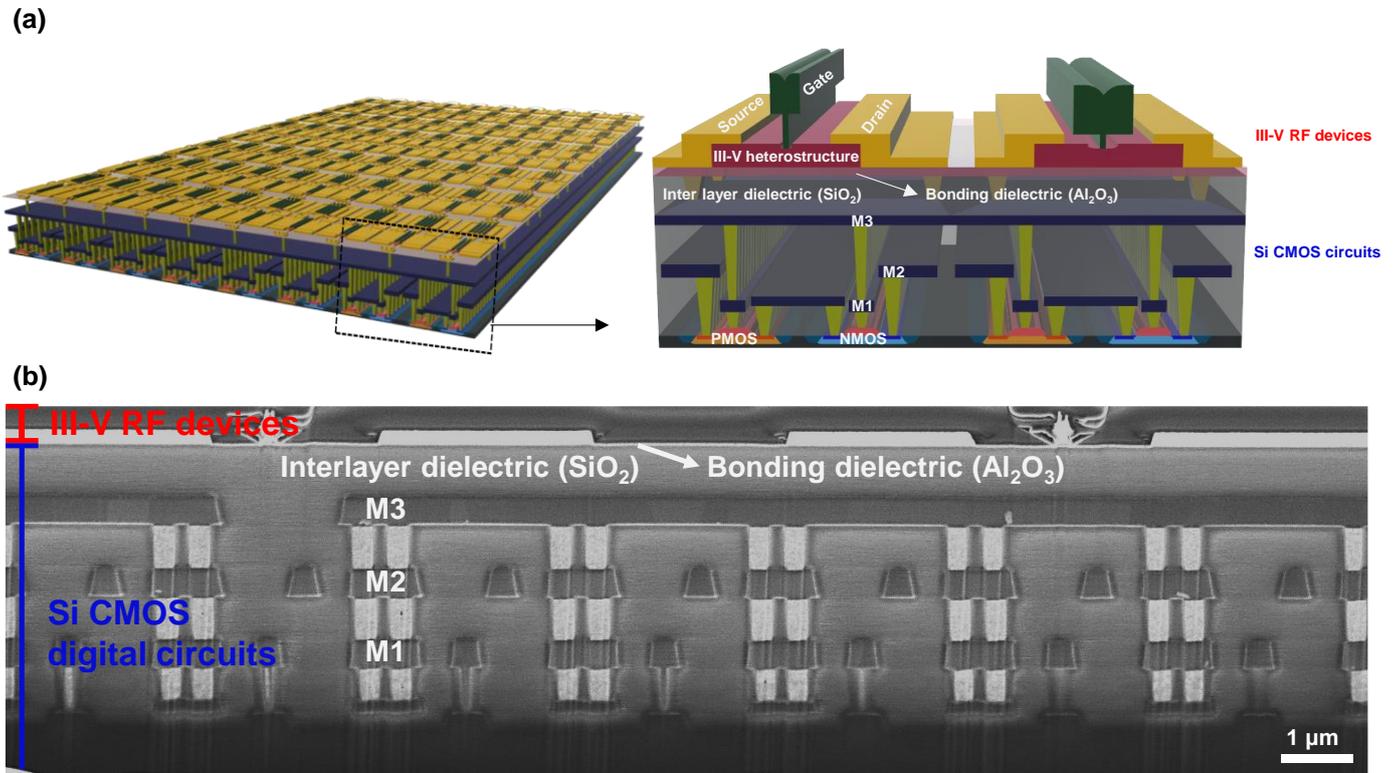


Figure 4. (a) Schematic of heterogeneous and monolithic 3D integrated III-V-based RF devices in Si CMOS. (b) Cross-sectional STEM image of top transistor based on InGaAs HEMT. Reprinted with permission from Ref. [10]. 2022, ACS Nano.

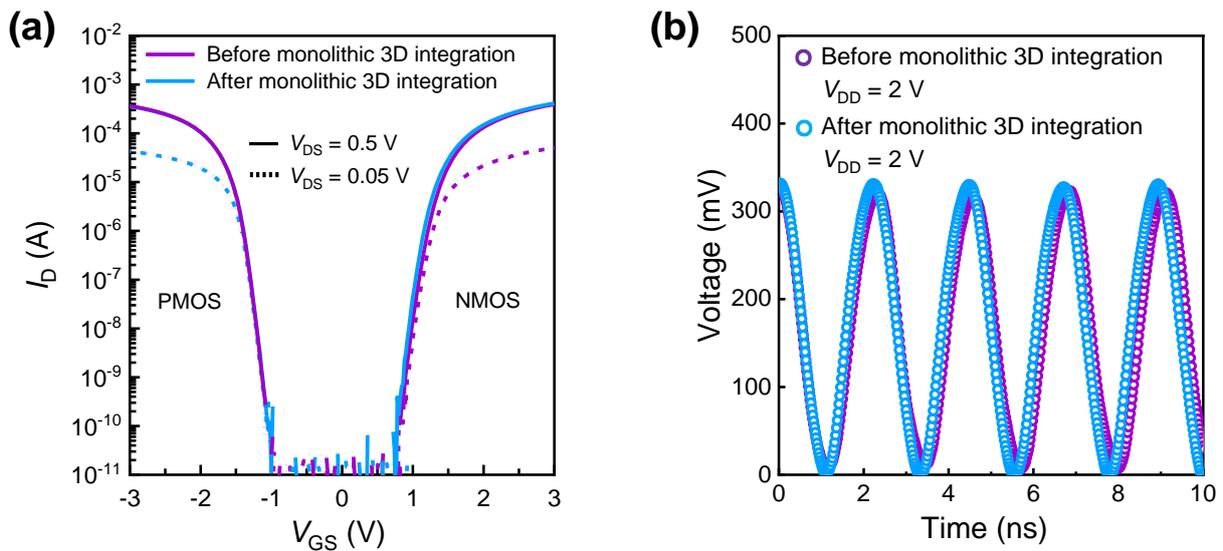


Figure 5. (a) Transfer characteristics of bottom single Si MOSFET before and after monolithic 3D integration. (b) Output waveform of VCO based on a ring oscillator composed of multiple Si MOSFETs. Reprinted with permission from Ref. [10]. 2022, ACS Nano.

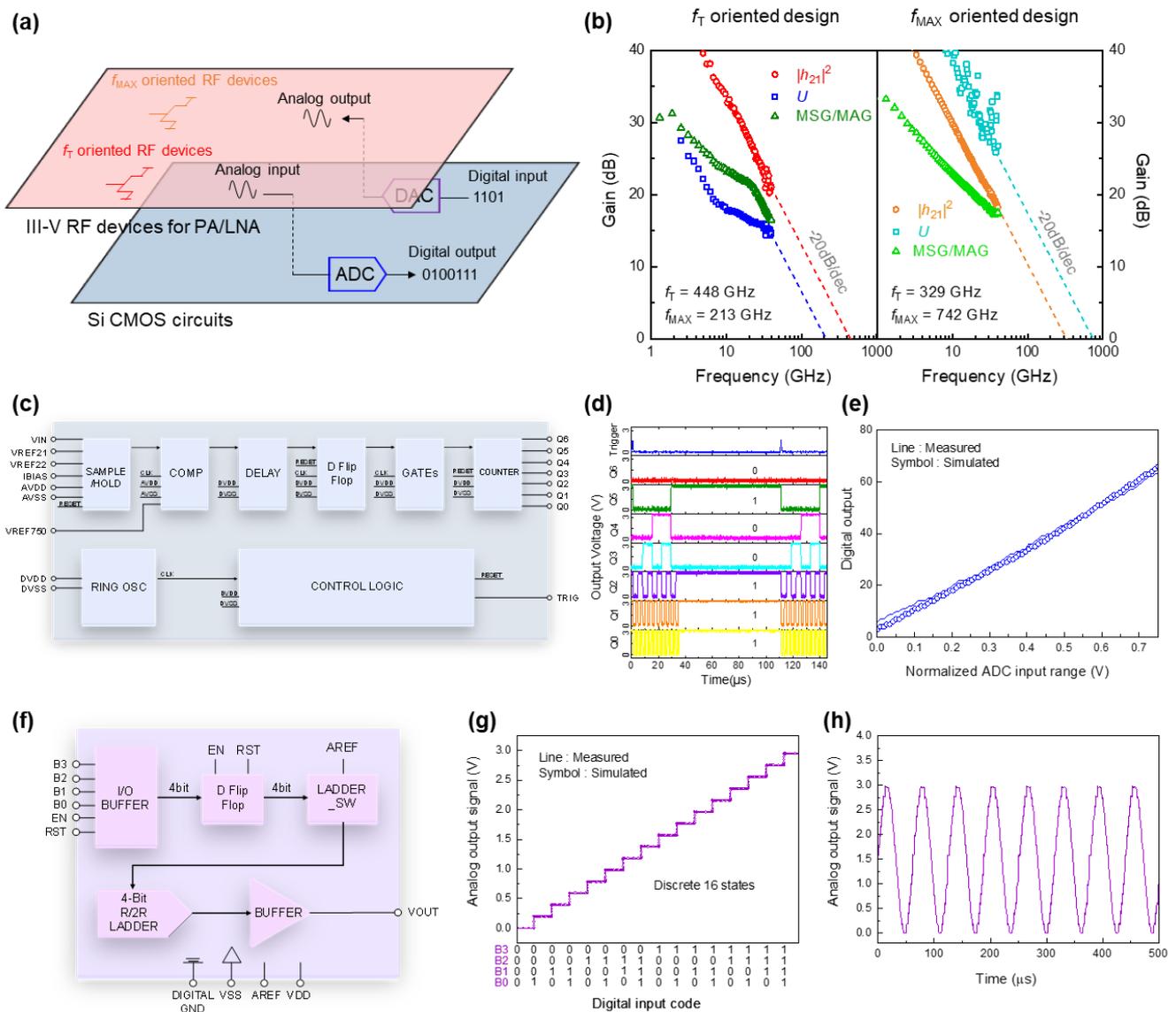


Figure 6. (a) Conceptual schematic of heterogeneous and monolithic 3D integrated III-V-based RF devices on Si CMOS. (b) Gain plot of f_T and f_{MAX} -oriented top InGaAs HEMTs. (c) The block diagram of ADC. (d) Time domain output voltage of ADC. (e) Digital output of ADC. (f) The block diagram of DAC. (g) Analog output of DAC. (h) Sinewave output of DAC. Reprinted with permission from Ref. [10]. 2022, ACS Nano.

2.3. Issues on Monolithic 3D Integrated Analog/RF-Digital Mixed-Signal IC

2.3.1. Substrate Digital Interference

One of the critical issues in analog/RF-digital mixed-signal integrated circuits is electromagnetic coupling [35,36]. The monolithic integration of analog/RF circuits and digital circuits in the same chip induces the crosstalk between them. Therefore, the appropriate shielding technology is essential. Representatively, there is substrate digital interference in mixed-signal IC. The substrate digital interference, which is caused by switching any digital circuits, can be spread across the shared substrate and degrade the performance of analog/RF circuits when the digital circuits and analog/RF circuits are integrated on the same substrate. Therefore, in the traditional Si-based analog/RF-digital mixed-signal circuits, shielding technology, such as guard ring, deep N-well, deep trench isolation, and through silicon via (TSV), has been necessarily used [37,38]. However, these approaches require many additional process steps and occupy an additional area, imposing critical costs and

area penalties. On the other hand, in the case of monolithic 3D integrated analog/RF-digital mixed-signal IC, the digital circuits and analog/RF circuits do not share the same substrate. These two different types of circuits are separated by an interlayer dielectric due to the inherent nature of the floating thin body structure of top devices. Therefore, it is expected that the digital interference from bottom digital circuits can be shielded and has no effect on top analog/RF circuits when an appropriate thickness of interlayer dielectric and BEOL lines are introduced.

To investigate the effect of substrate coupled digital interference in both conventional and monolithic 3D mixed-signal IC, we used a 31-stage ring oscillator in digital circuits as a signal source and a single transistor to sense the substrate digital interference in analog/RF circuits, as shown in Figure 7a. The schematics of the conventional and monolithic 3D mixed-signal systems are shown in Figure 7b,c. The top RF devices and bottom Si CMOS BEOL are separated with a 600-nm-thick interlayer dielectric. The results of substrate digital interference analysis are shown in Figure 7d,e. In the case of M3D mixed-signal IC, the bottom digital interference cannot propagate to the top circuits through the substrate because the digital and analog/RF circuits do not share the same substrate, whereas conventional 2D integrated transistors with the digital circuits strongly feel the digital interference when the digital circuits operate as in Figure 7d. This is another strong advantage of the M3D integration in mixed-signal IC.

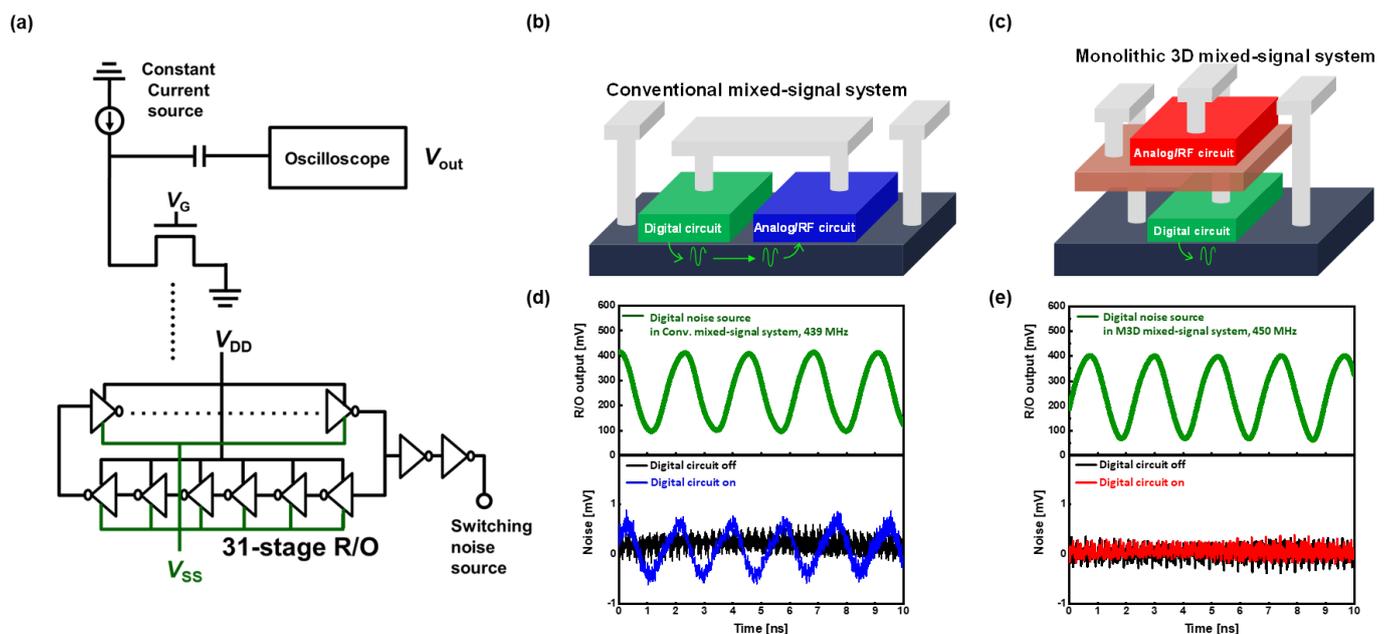


Figure 7. (a) Substrate digital interference measurement setup. The schematic of (b) conventional and (c) monolithic 3D integrated digital-analog/RF mixed-signal IC. The result of substrate digital interference analysis in (d) conventional and (e) monolithic 3D integrated digital-analog/RF mixed-signal IC. Reprinted with permission from Ref. [11]. 2021, JSAP.

2.3.2. Self-Heating

Another critical issue in monolithic 3D systems is the self-heating of top devices, which can affect the device's performance. As reported by many research groups, the top devices are thermally isolated by an interlayer dielectric which has a low thermal conductivity, thereby, the performance and reliability can be degraded [39,40]. In the monolithic 3D system, the self-heating of the top device is one of the limiting factors in high performance, hence, many groups have reported on the self-heating effect in the M3D systems [39,40]. We presented one of the possible solutions to relaxing self-heating by introducing the metal plate, which has a high thermal conductivity at the backside of the top RF devices, as shown in Figure 8a [41,42]. The embedded metal can act as an

additional heat dissipation path because the metal has high thermal conductivity. We used high-resolution thermoreflectance microscopy (TRM) to investigate the self-heating during the transistor operation [41,43]. Since variation in relative reflectivity ($\Delta R/R$) has a linear relationship with variation in surface temperature (ΔT), the temperature of the device can be determined by detecting the change in reflectivity(R). The real-time thermal distribution of 3D integrated InGaAs-based RF transistors with different structures is shown in Figure 8b–e.

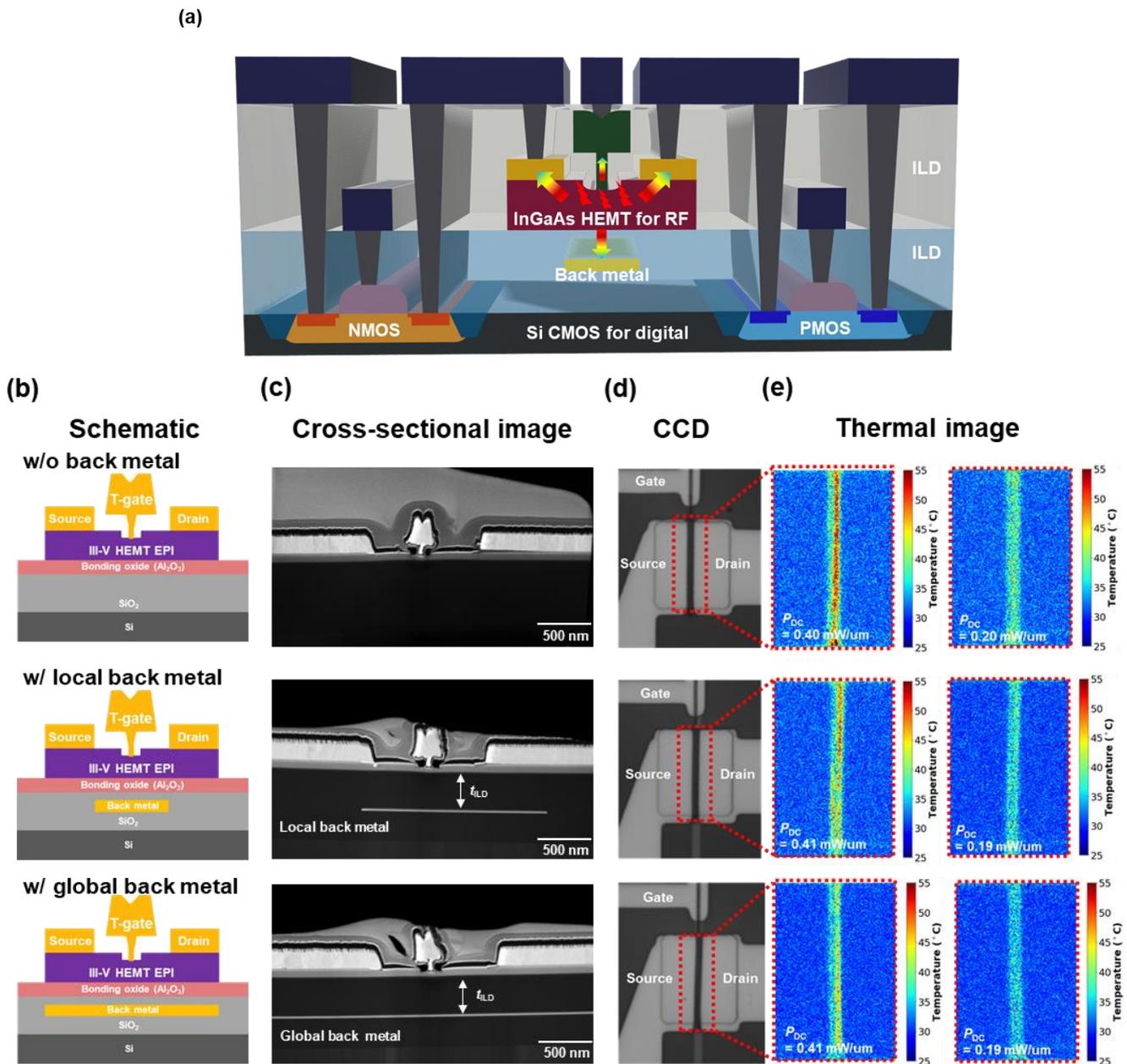


Figure 8. (a) Conceptual schematic of heterogeneous and monolithic 3D integrated III-V-based RF device on Si CMOS with back metal to relax the self-heating of top devices. The arrows represent the heat spread. The (b) schematics, (c) cross-sectional images, (d) CCD, and (e) thermal images of 3D integrated InGaAs HEMTs with different structures. Reprinted with permission from Ref. [41]. 2022, IEEE.

The 3D integrated InGaAs HEMTs with back metal show reduced self-heating characteristics compared to the 3D integrated InGaAs HEMTs without back metal because the back metal with high thermal conductivity offers an additional heat dissipation path, resulting in low static device temperature. The self-heating relaxing effect of the top devices

increased as the size of the back metal increased, and the distance from the top device to the back metal decreased. However, the additional back parasitic capacitance is caused by the back metal. Moreover, when the metal is introduced near the top devices to relax the self-heating, the effect of back capacitance becomes more important, requiring careful device design to mitigate this trade-off relationship. The influence of the back metal on the RF performance of top devices was investigated [41]. However, a more systematic investigation of the influence of the back metal on the top RF devices in the M3D platform will be needed for successful heterogeneous and monolithic 3D integrated RF SoC.

2.4. Benchmarking of the Monolithic 3D Integrated RF Transistors

Many research groups have developed monolithic 3D integrated RF transistors. Figure 9 and Table 1 show the RF performance and information of the process to compare the state-of-the-art 3D integrated RF transistors [10,12–14,44–48]. The most important metric is cutoff frequency because it determines the maximum frequency at which the device can be used. As shown in Figure 9 the III-V-based RF devices, especially InGaAs-based RF transistors, obviously outperform Si transistors. This would motivate the heterogeneous and monolithic 3D integration in future wireless communication. Furthermore, the RF performance versus power consumption of the monolithic 3D integrated InGaAs on Si and monolithic 3D integrated Si on Si are shown in Figure 9. The monolithic 3D integrated InGaAs-based RF transistors on Si show higher RF performance at the same power consumption or less power consumption at the same RF performance than monolithic 3D integrated Si-based RF transistors on Si. This characteristic is also very important to be used for cryogenic LNA toward scalable quantum computing [49]. One drawback would be the fact that InGaAs-based devices are still difficult to be grown on large substrates, such as 200 or 300 mm sizes, resulting in a size mismatch to Si CMOS technology. The GaN-based devices overcome this problem by growing the GaN on Si wafers, but their RF performances fall short of InGaAs-based devices. Even in the case of InGaAs, it is thought that this problem can also be solved by introducing the growth of III-V on Si substrate or die to wafer bonding [50–52].

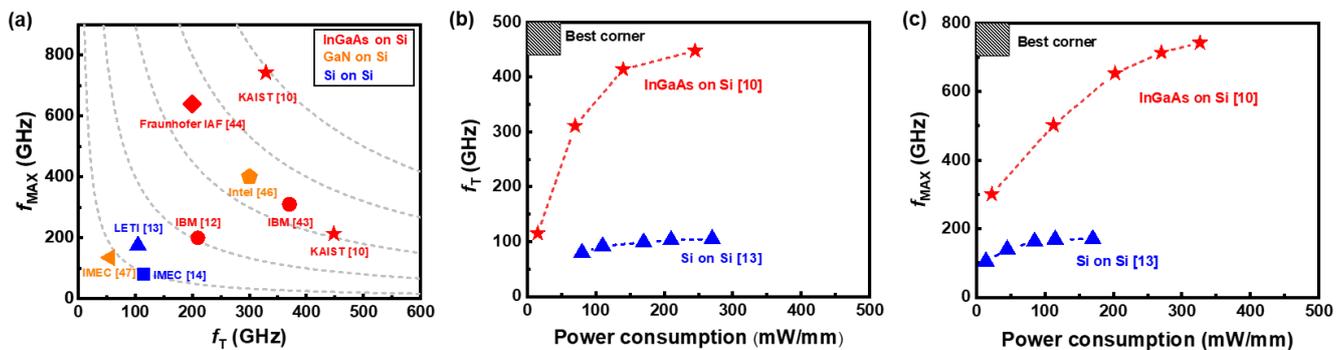


Figure 9. (a) The important FOMs of f_T and f_{MAX} are shown with different types of state-of-the-art monolithic 3D RF transistors. The (b) f_T and (c) f_{MAX} versus power consumption of InGaAs on Si and Si on Si. The best performances of each technology were used for comparison.

Table 1. Comparison of M3D RF transistors.

RF Device	T _{process of RF Device}	L_G	f_T/f_{MAX}	$\sqrt{f_T f_{MAX}}$	Integration with Si CMOS
KAIST [10]	$\leq 300\text{ }^\circ\text{C}$	80 nm (f_{MAX} oriented design)	329/742 GHz	494 GHz	Yes
		140 nm (f_T oriented design)	448/213 GHz	309 GHz	

Table 1. Cont.

	RF Device	T _{process} of RF Device	L _G	f _T /f _{MAX}	$\sqrt{f_T \cdot f_{MAX}}$	Integration with Si CMOS
IBM [43]	InGaAs MOSFET	≤500 °C	20 nm	380/310 GHz	343 GHz	No
IBM [12]	InGaAs MOSFET	≤500 °C	25 nm	210/200 GHz	205 GHz	Yes
Fraunhofer IAF [44]	InGaAs MOSHEMT	≤300 °C	20 nm	640/200 GHz	358 GHz	No
NUS [45]	InGaAs MOSHEMT	≤350 °C	150 nm	60/- GHz	-	Yes
Intel [46]	GaN MOSHEMT	-	30 nm	300/400 GHz	346 GHz	Yes
IMEC [47]	GaN HEMT	-	110 nm	56/135 GHz	87 GHz	No
IMEC [14]	Si MOSFET	≤525 °C	80 nm	80/115 GHz	96 GHz	No
LETI [13]	Si MOSFET	≤500 °C	45 nm	105/175 GHz	136 GHz	No

3. M3D Integration for High-Resolution III-V Image Sensors

Other than RF-SoCs, image sensors are one of the important applications for obtaining visual information in an autonomous car, time-of-flight sensors, and industrial surveillance systems [53–55]. Recently, 3-dimensional packaging using through-Si vias (TSVs) technology has been used to develop high-speed and high-resolution image sensors based on visible light absorption [56]. It is because there are several advantages, such as small chip size, high fill factor, and high bandwidth, whereas the conventional planar integration method, which places pixel region and pixel transistors and circuit section on the same plane, reduces the pixel area and an increases chip size, as shown in Figure 10 [5,57].

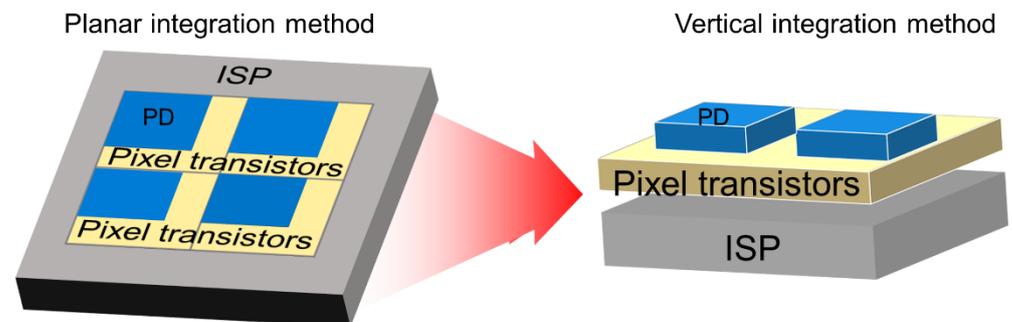


Figure 10. The development trend for fabricating image sensors from conventional planar integration method to newly 3D vertical integration including pixel area, pixel transistors, and image signal processor (ISP).

Although packaging technology has greatly accelerated the performance of image sensors, there is still room for improvement by full 3D integration with pixel transistors, etc. Therefore, ultimately, M3D integration can be a viable approach for future image sensors requiring much more functionalities. Beyond the visible light, detection of the short-wavelength infrared (SWIR) light has become increasingly important, which is mostly accomplished with the III-V material-based photodetectors (PDs) [55,56]. The packaging-based hybrid integration method currently used in III-V device integration with Si ICs has obvious limitations in terms of the resolution of several μm [56]. Thus, the benefits of M3D integration can be maximized in fabricating III-V image sensors because III-V materials can be processed at low temperatures, even a room temperature, and can be separated from donor substrates, making them very suitable for sequential fabrication [58,59]. Moreover,

III-V thin film-based pixels can provide broadband detection capabilities with simple structure design, such as TMD/III-V heterojunction, Metal/III-V Schottky junction, III-V with optical mode resonance structure, etc. [60–62].

Here, we demonstrated the M3D integration of III-V-based PDs on SOI pixel transistors using CMOS-compatible fabrication processes, such as wafer-bonding and low-temperature sequential fabrication processes.

3.1. InGaAs Photodetectors on SOI-MOSFETs by Using Monolithic Integration and Sequential Fabrication Process

Figure 11 depicts the entire fabrication process flow for M3D InGaAs PDs on SOI-MOSFETs. SOI-MOSFETs have 50-nm Si channel thickness, 365-nm-thick BOX, and TiN/HfAlO_x gate stack with a conventional InGaAs PD structure. Additionally, a chemical-mechanical polishing (CMP) process was used to obtain a flat surface for wafer bonding by depositing RF-sputtered SiO₂ inter-layer dielectric (ILD) on SOI-MOSFET. The InGaAs PD structure was then bonded to SOI-MOSFETs by utilizing an intermediate layer of 40-nm-thick Al₂O₃ layer with oxygen plasma treatment. Then, the sequential fabrication process of InGaAs PD on SOI-MOSFET with various mesa dimensions was performed, indicating pixel pitch scalability of InGaAs PDs. We used the room-temperature process for M3D integration here, even without the contact annealing process of PDs. Finally, as shown in Figure 11h, the interconnection between InGaAs PD cathode and the source region of SOI-MOSFET was performed for 1 pixel/1-pixel transistor operation.

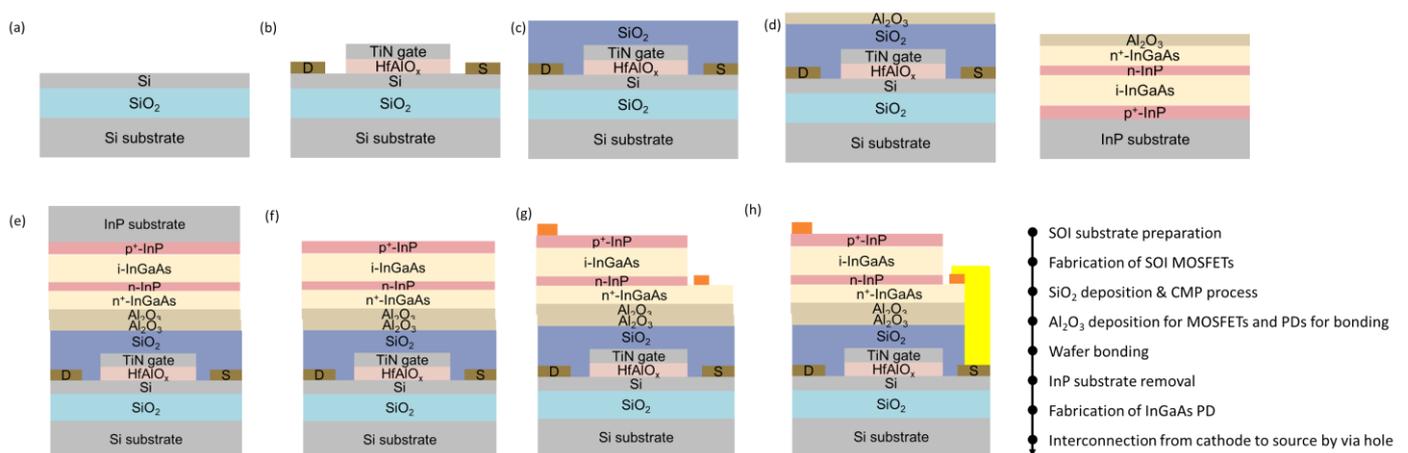


Figure 11. The fabrication process of vertically integrated InGaAs PDs on SOI-MOSFETs. (a) SOI substrate preparation. (b) Fabrication of SOI MOSFETs with TiN gate and HfAlO_x. (c) SiO₂ deposition and CMP process for planarization. (d) Al₂O₃ deposition for MOSFETs and PDs for wafer bonding. (e) Wafer bonding with plasma treatment. (f) InP substrate removal by using HCl solution. (g) Sequentially processed InGaAs PDs. (h) Interconnection from cathode of PDs to sources of MOSFETs by filling via holes. Reprinted with permission from Ref. [15]. 2020, IEEE.

Figure 12a shows a low-magnification transmission electron microscopy (TEM) image of the M3D-integrated InGaAs PD on the SOI-MOSFET structure. Bottom SOI-MOSFET and top InGaAs PD layers were clearly seen to be free of voids and dislocations, indicating integration stability with only a low process temperature. Furthermore, the inset photograph of Figure 12a exhibits the actual fabrication of InGaAs PD on the 2 cm × 2 cm SOI-MOSFET chip with various dimensions of PD devices. These devices were formed by using a sequential fabrication process on the SOI-MOSFETs, implying that pixel pitch scaling could be facilitated by a lithographic alignment due to the elimination of a mechanical alignment used in TSVs and hybrid integration methods. In addition, energy dispersive X-ray (EDX) spectroscopy analysis was performed along with the red arrow, as shown in Figure 12a, to evaluate the bonding interface. The resulting EDX line profile was shown

in Figure 12b for various atoms. We observed the formation of abrupt interfaces between different materials of InGaAs/Al₂O₃ and Al₂O₃/SiO₂, suggesting our fabrication steps did not induce any interdiffusion of elements due to the low-temperature process.

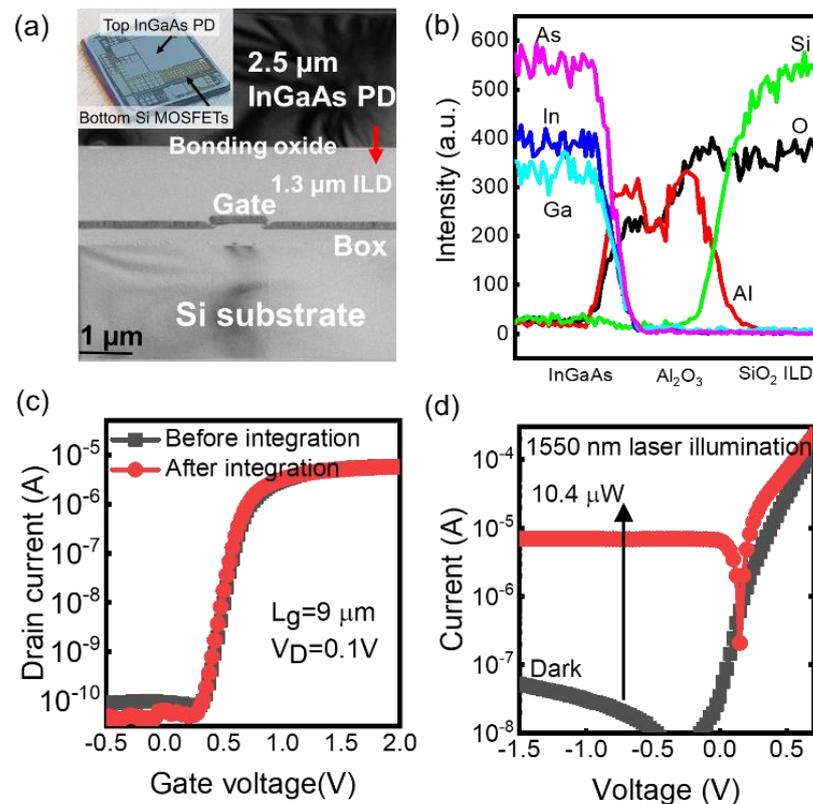


Figure 12. (a) Cross-sectional low-magnified TEM image of InGaAs PDs on SOI-MOSFETs with SiO₂ ILD layer and inset photograph for an actual chip. The red arrow is the EDX scan line. (b) EDX line profile of various atoms of In, Ga, As, Si, O, and Al along to the red arrow in Figure 11a. (c) The transfer curves of SOI-MOSFET with 9- μ m gate length before and after monolithic 3D integration. (d) Current-voltage characteristics of InGaAs PD with a 1550-nm laser under dark/light conditions. The current is increased after laser illumination. Reprinted with permission from Ref. [15]. 2022, IEEE.

Then, we performed the electrical and optical characterization of each device, as shown in Figure 12c,d, to confirm device performances of InGaAs PDs and SOI-MOSFETs before and after the M3D integration process. Figure 12c illustrates the transfer curves of the 9- μ m gate length SOI-MOSFET with and without the M3D integration process. This evaluation is highly significant because the fabrication process of top layer devices can affect the bottom devices during the thermal processes and plasma process, etc. In our devices, there is a negligible difference in the subthreshold swing (S.S), on/off ratio, and saturation current of SOI-MOSFETs before and after M3D integration. It was confirmed that the top InGaAs devices process and integration process do not degrade the performance of the bottom devices. Moreover, the integrated InGaAs PD device has a good current ratio at ± 1.5 V, corresponding to approximately 10^4 under dark conditions. Figure 12d shows a clear photoresponse with 0.7 A/W of responsivity without anti-reflection coating (ARC) obtained with 1550-nm laser illumination at the surface. From these results, top and bottom device qualities would be well preserved during the thin-film transfer process, and the device fabrication process that indicated the proposed M3D integration could be used to fabricate an actual M3D image sensor with a high resolution and a small chip size.

3.2. Evaluation of Fabricated InGaAs Photodetectors on SOI-MOSFETs for Mimicking IC Operation

Finally, we investigated the readout function for mimicking the actual ROIC operation using M3D integrated InGaAs PDs on SOI-MOSFETs. In actual ROIC operation, Figure 13a illustrates the fundamental building block of typical circuit configurations, such as direct injection and source-follower per detector [63]. Although IC operation mechanisms vary in many configurations, the basic element close to PDs is a simple combination of 1 PD and 1 Tr. Thus, we evaluated the fundamental function of IC operation in M3D integrated InGaAs PDs on SOI-MOSFETs (1PD and 1Tr structure). The readout voltage (V_{out}) measurement was performed for the top InGaAs PD layer under the illumination condition of a 1550 nm laser. Figure 13b shows the resulting V_{out} as a function of the light intensity by varying the gate bias (V_{GS}) from 0.425 V to 1 V, where 0.425 V of V_{GS} is in the subthreshold regime. This is due to the SOI-MOSFETs' ability to function as a charge transfer gate in direct injection mode, where photo-generated carriers are directly injected via the source on the output stage. V_{out} gradually increased as V_{GS} increased from 0.4 V to 1 V, which could be attributed to the division of resistance between Tr and PD caused by the Tr resistance decrease. Furthermore, in fixed V_{GS} , increasing light intensity from 0.1 to 10 μW resulted in the V_{out} decrease due to PD resistance decrease. These results suggested the successful mixed-signal operation of the direct injection mechanism of ROIC by using M3D integrated PD and Tr structure. Recently, we demonstrated an M3D integrated MicroLED display on CMOS driver IC with a low-temperature process [17]. This integration process could be directly applied to integrated PD on ROIC in the future.

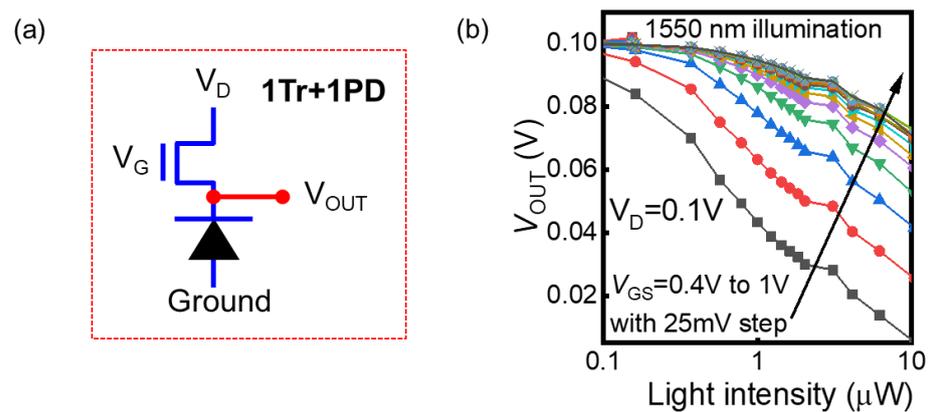


Figure 13. (a) The measured unit cell for readout operation for the fabricated InGaAs PD on SOI-MOSFET for mimicking the direct injection operation. (b) Electrical responses of the measured unit cell with various gate biases and light intensity on top InGaAs PDs. Reprinted with permission from Ref. [15]. 2022, IEEE.

4. Conclusions

We presented the M3D integration-based InGaAs HEMTs and InGaAs PDs on Si-based bottom devices/ICs for next-generation RF and image sensor applications. For the RF applications, we demonstrated the heterogenous and monolithic 3D integration of III-V RF devices on Si CMOS circuits, which enable performance optimization in both RF and digital integrated circuits. Furthermore, we discussed the issues and solutions of substrate digital interference and self-heating in terms of the M3D integrated RF platform. For the image sensor applications, to overcome the inherent limitation of hybrid integration technology for fabricating high-resolution SWIR image sensors, the integrated 1 PD and 1 Tr devices successfully exhibited good PD performances after the layer transfer and fabrication process without bottom Si device degradations. Photolithographic alignment allowed dimension scaling, which can scale the pixel pitch to high-resolution ($<1 \mu\text{m}$). Furthermore, the basic IC operation changing from light signals to electrical signals was achieved. These results strongly suggested that the heterogeneous and monolithic 3D integration will provide high performance and multi-functionality in various applications, such as RF and image sensors.

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